

# Conservation Scheme for sigma Ocean Models

(Finite Volume Consideration for Pressure  
Gradient Force )

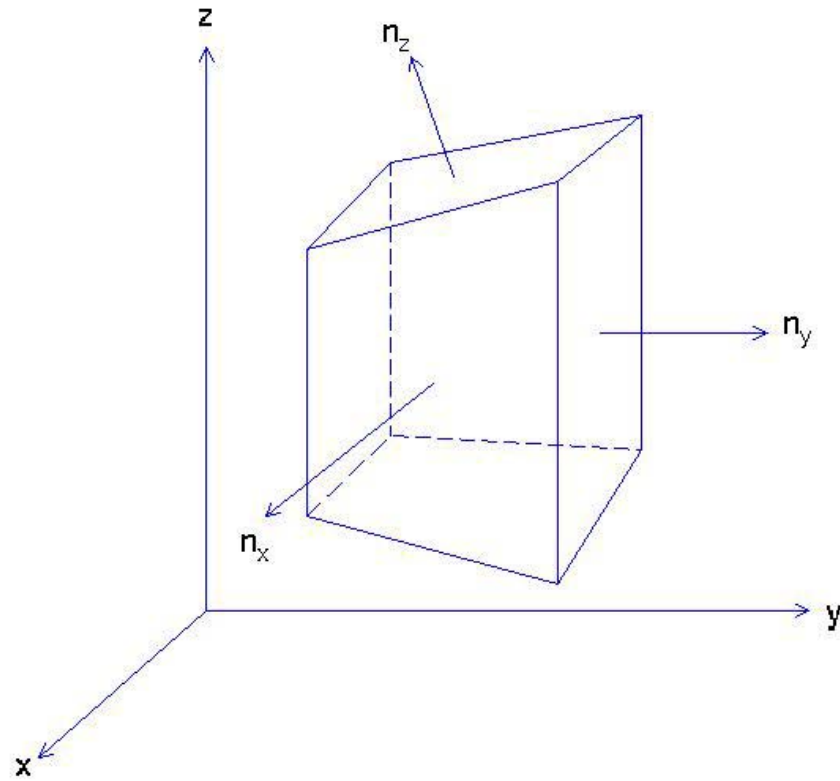
Peter C Chu and Chenwu Fan  
Naval Postgraduate School  
Monterey, California, USA

AMS 5<sup>th</sup> Conference on Coastal Atmospheric and Oceanic  
Prediction and Processes, Seattle, Aug. 6-8, 2003

# Four Types of Numerical Models

- Spectral Model (not suitable for oceans due to irregular lateral boundaries)
- Finite Difference (z-coordinate, sigma-coordinate, ...)
- Finite Element
- Finite Volume

# Finite Volume



# Finite Volume Model

- Transform of PDE to Integral Equations
- Solving the Integral Equation for the Finite Volume
- Flux Conservation

# Dynamic and Thermodynamic Equations

- Continuity  $\nabla \cdot (\rho \mathbf{V}) = 0$
- Momentum

$$\frac{\partial(\rho \mathbf{V})}{\partial t} + \nabla \cdot (\rho \mathbf{V} \mathbf{V}) = -\nabla p + \nabla \cdot (\mu \nabla \mathbf{V}) + \mathbf{F}$$

- Thermodynamic

$$\frac{\partial \phi}{\partial t} + \nabla \cdot (\mathbf{V} \phi) = \nabla \cdot (\kappa_{\phi} \nabla \phi) + F_{\phi}$$

# Integral Equations for Finite Volume

- Continuity 
$$\int_{\Omega} \nabla \cdot (\rho \mathbf{V}) d\Omega = \oint_{\Gamma} \rho \mathbf{V} \cdot \mathbf{n} d\Gamma = 0$$

- Momentum

$$\int_{\Omega} \frac{\partial(\rho \mathbf{V})}{\partial t} d\Omega + \oint_{\Gamma} \rho \mathbf{V} \mathbf{V} \cdot \mathbf{n} d\Gamma = - \oint_{\Gamma} p d\Gamma + \oint_{\Gamma} \mu \nabla \mathbf{V} \cdot \mathbf{n} d\Gamma + \int_{\Omega} \mathbf{F} d\Omega \quad \Omega$$

- Thermodynamic

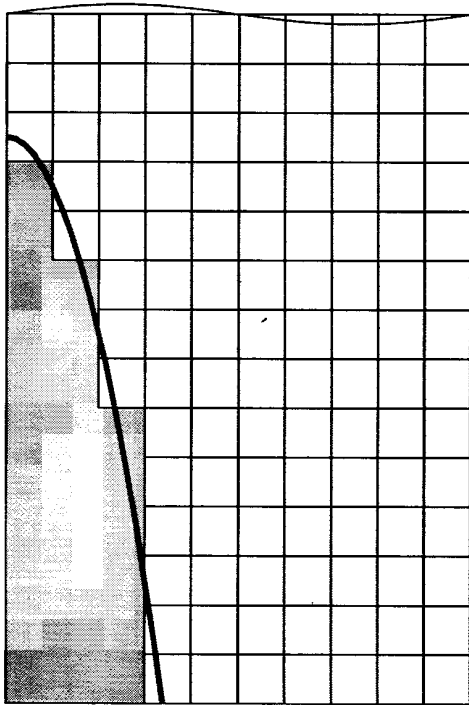
$$\int_{\Omega} \frac{\partial \phi}{\partial t} d\Omega + \oint_{\Gamma} \phi \mathbf{V} \cdot \mathbf{n} d\Gamma = \oint_{\Gamma} \kappa_{\phi} \nabla \phi \cdot \mathbf{n} d\Gamma + \int_{\Omega} F_{\phi} d\Omega$$

# Time Integration of Phi-Equation

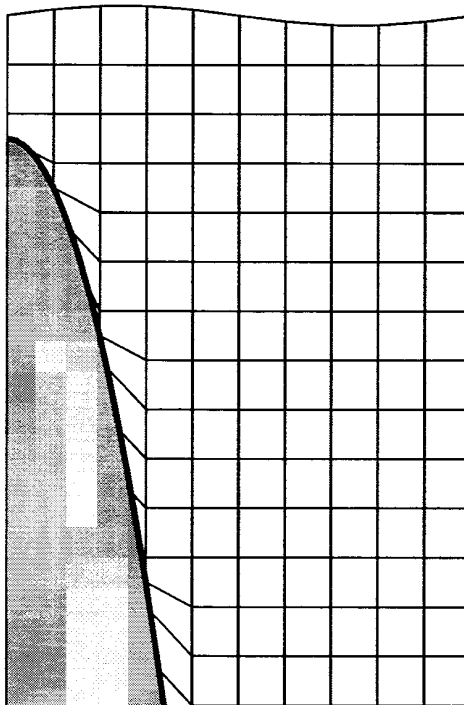
$$\int_{\Omega} \phi(t_2) d\Omega - \int_{\Omega} \phi(t_1) d\Omega = - \Delta t \oint_{\Gamma} \phi(t^*) \mathbf{V} \cdot \mathbf{n} d\Gamma$$
$$+ \Delta t \oint_{\Gamma} \kappa_{\phi} \nabla \phi(t^*) \cdot \mathbf{n} d\Gamma + \Delta t \int_{\Omega} F_{\phi}(t^*) d\Omega -$$

# Comparison Between Finite Difference (z- and sigma-coordinates) and Finite Volume Schemes

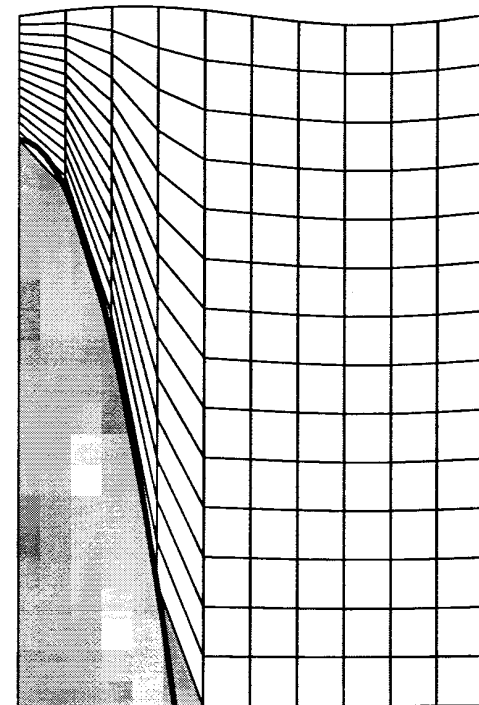
z - Coordinate



FVM



$\sigma$  - Coordinate





# CFL Condition

$$U \Delta x / \Delta t < 1$$

Easily to identify in z-coordinate and finite volume models.

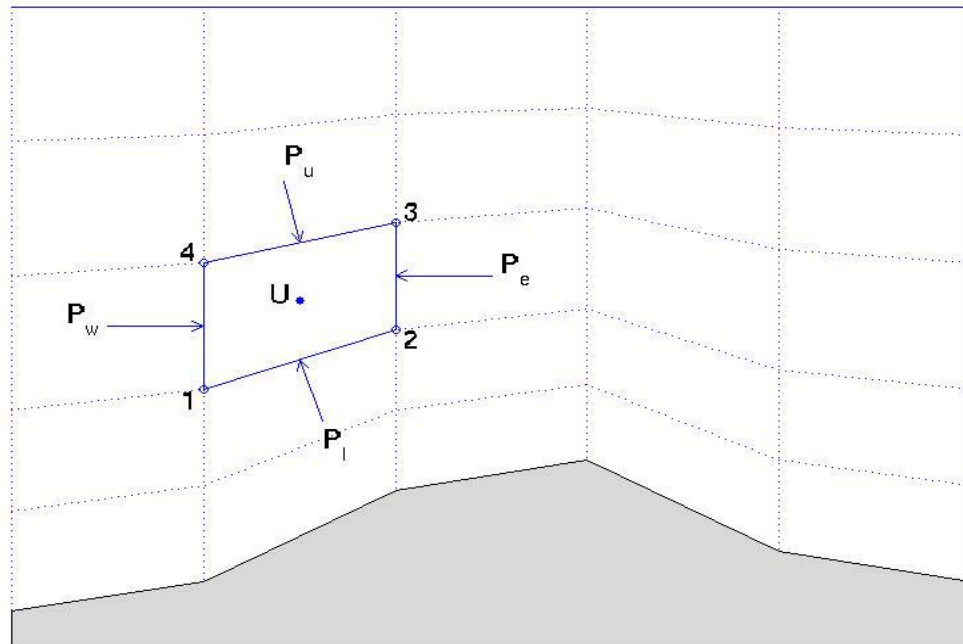
Hard to identify in sigma-coordinate model

# How to reduce errors with low computer cost?

## Hydrostatic Correction

- Chu, P.C., and C.W. Fan, 2003: Hydrostatic correction for reducing horizontal pressure gradient errors in sigma coordinate models. *Journal of Geophysical Research*, J. Geophys. Res. Vol. 108, No. C6, 3206, [10.1029/2002JC001668](https://doi.org/10.1029/2002JC001668).

# Finite Volume Consideration



$$\mathbf{F} = L_y \oint_C p \mathbf{n} ds$$

# Horizontal Pressure Gradient

$$\frac{\partial p}{\partial x} \equiv \frac{F_x}{L_y \Delta S} = -\frac{1}{\Delta S} \left( \int_1^2 p_l dz + \int_2^3 p_e dz + \int_3^4 p_u dz + \int_4^1 p_w dz \right)$$

# Second-Order Scheme

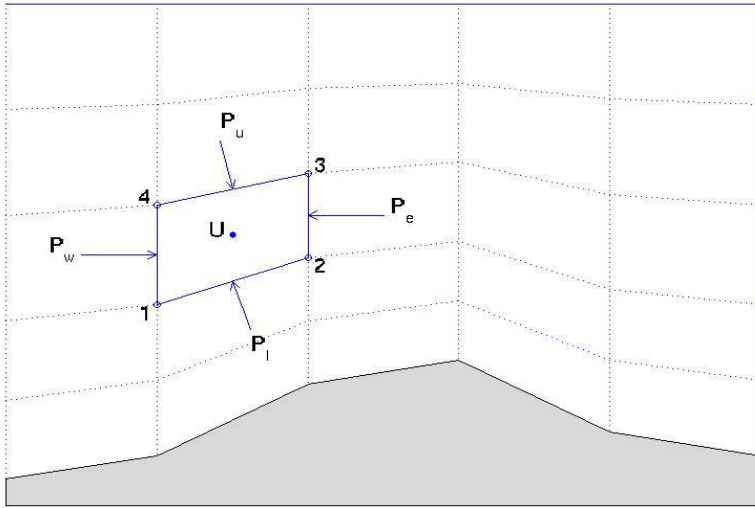
$$\frac{\Delta p}{\Delta x} = \frac{1}{\Delta S} \left[ \bar{p}_l(z_{i+1,k+1} - z_{i,k+1}) + \bar{p}_e(z_{i+1,k} - z_{i+1,k+1}) \right. \\ \left. + \bar{p}_u(z_{i,k} - z_{i+1,k}) + \bar{p}_w(z_{i,k+1} - z_{i,k}) \right]$$

$$\int_1^2 p_l dz = \bar{p}_l(z_{i+1,k+1} - z_{i,k+1}), \quad \int_2^3 p_e dz = \bar{p}_e(z_{i+1,k} - z_{i+1,k+1}),$$

$$\int_3^4 p_l dz = \bar{p}_u(z_{i,k} - z_{i+1,k}), \quad \int_4^1 p_w dz = \bar{p}_w(z_{i,k+1} - z_{i,k}),$$

$$\left( \frac{\Delta p}{\Delta x} \right)_{i,k} = \frac{(p_{i+1,k+1} - p_{i,k})(H_{i+1}\sigma_k - H_i\sigma_{k+1}) + (p_{i+1,k} - p_{i,k+1})(H_i\sigma_k - H_{i+1}\sigma_{k+1})}{\Delta x_i \Delta \sigma_k (H_i + H_{i+1})}$$

# Steep Topography – Hermit Polynomial Integration



$$\xi = \frac{l - l_1}{\Delta l}, \quad \Delta l \equiv l_2 - l_1$$

$$\int_{l_1}^{l_2} p(l) dl = \Delta l \int_0^1 \Psi(\xi) d\xi$$

# Hermit Polynomial Integration

$$\int_{l_1}^{l_2} p dl = \int_0^1 \Psi(\xi) d\xi = \frac{\Delta l}{2} (p_1 + p_2) + \frac{\Delta l^2}{12} \left( \left( \frac{\partial p}{\partial l} \right)_1 - \left( \frac{\partial p}{\partial l} \right)_2 \right)$$

$$\Psi(\xi) = p_{l_1} \Phi_1 + p_{l_2} \Phi_2 + \Delta l \left( \frac{\partial p}{\partial l} \right)_{l_1} \Phi_3 + \Delta l \left( \frac{\partial p}{\partial l} \right)_{l_2} \Phi_4$$

$$\Phi_1 = 1 - 3\xi^2 + 2\xi^3, \quad \Phi_2 = 3\xi^2 - 2\xi^3,$$

$$\Phi_3 = \xi - 2\xi^2 + \xi^3, \quad \Phi_4 = \xi^3 - \xi^2$$

# Hydrostatic Correction

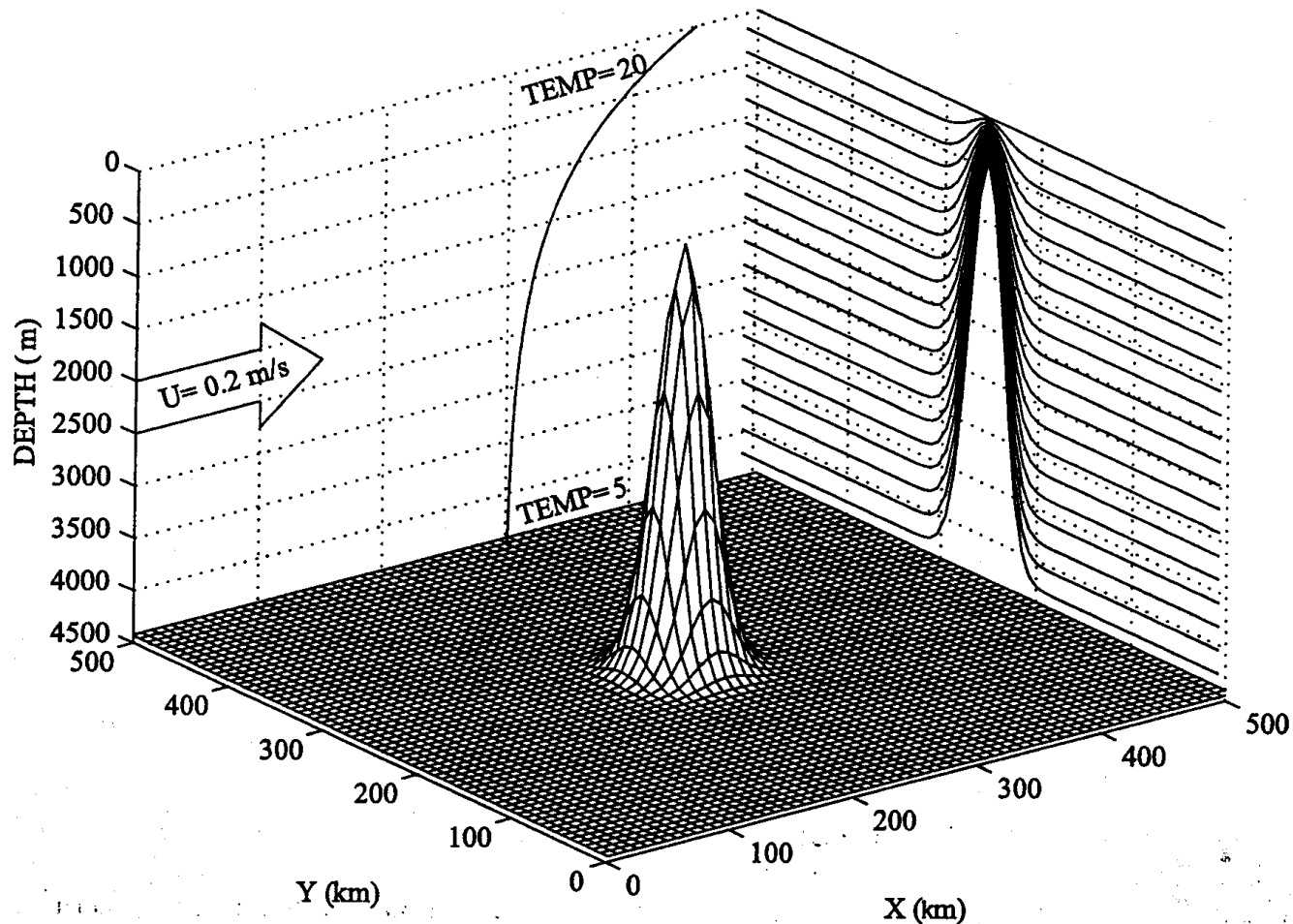
$$\left(\frac{\Delta p}{\Delta x}\right)_{i,k} \simeq \frac{\left[ (p_{i+1,k+1} - p_{i,k})(z_{i+1,k} - z_{i,k+1}) + (p_{i+1,k} - p_{i,k+1})(z_{i,k} - z_{i+1,k+1}) \right]}{(x_{i+1} - x_i)(z_{i,k} + z_{i+1,k} - z_{i,k+1} - z_{i+1,k+1})} + \Omega_{ik}$$

$$\Omega_{ik} = \frac{g\Gamma_{ik}}{6(x_{i+1} - x_i)(z_{i,k} + z_{i+1,k} - z_{i,k+1} - z_{i+1,k+1})},$$

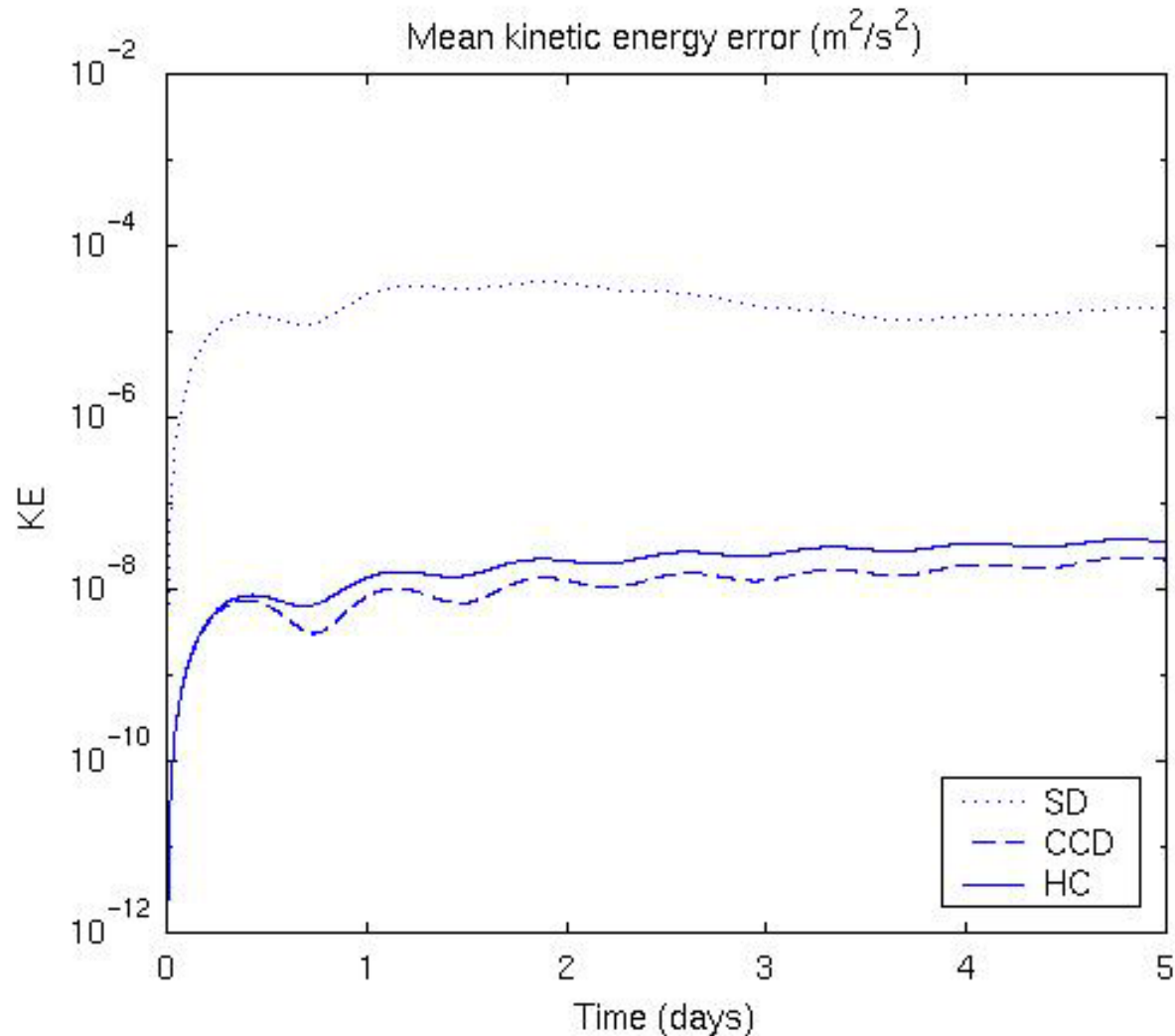
$$\Gamma_{ik} \equiv \left[ (H_{i+1}\sigma_k - H_{i+1}\sigma_{k+1})^2 (\rho_{i+1,k} - \rho_{i+1,k+1}) - (H_i\sigma_k - H_i\sigma_{k+1})^2 (\rho_{i,k} - \rho_{i,k+1}) \right. \\ \left. + (H_{i+1}\sigma_{k+1} - H_i\sigma_{k+1})^2 (\rho_{i+1,k+1} - \rho_{i,k+1}) - (H_{i+1}\sigma_k - H_i\sigma_k)^2 (\rho_{i+1,k} - \rho_{i,k}) \right]$$

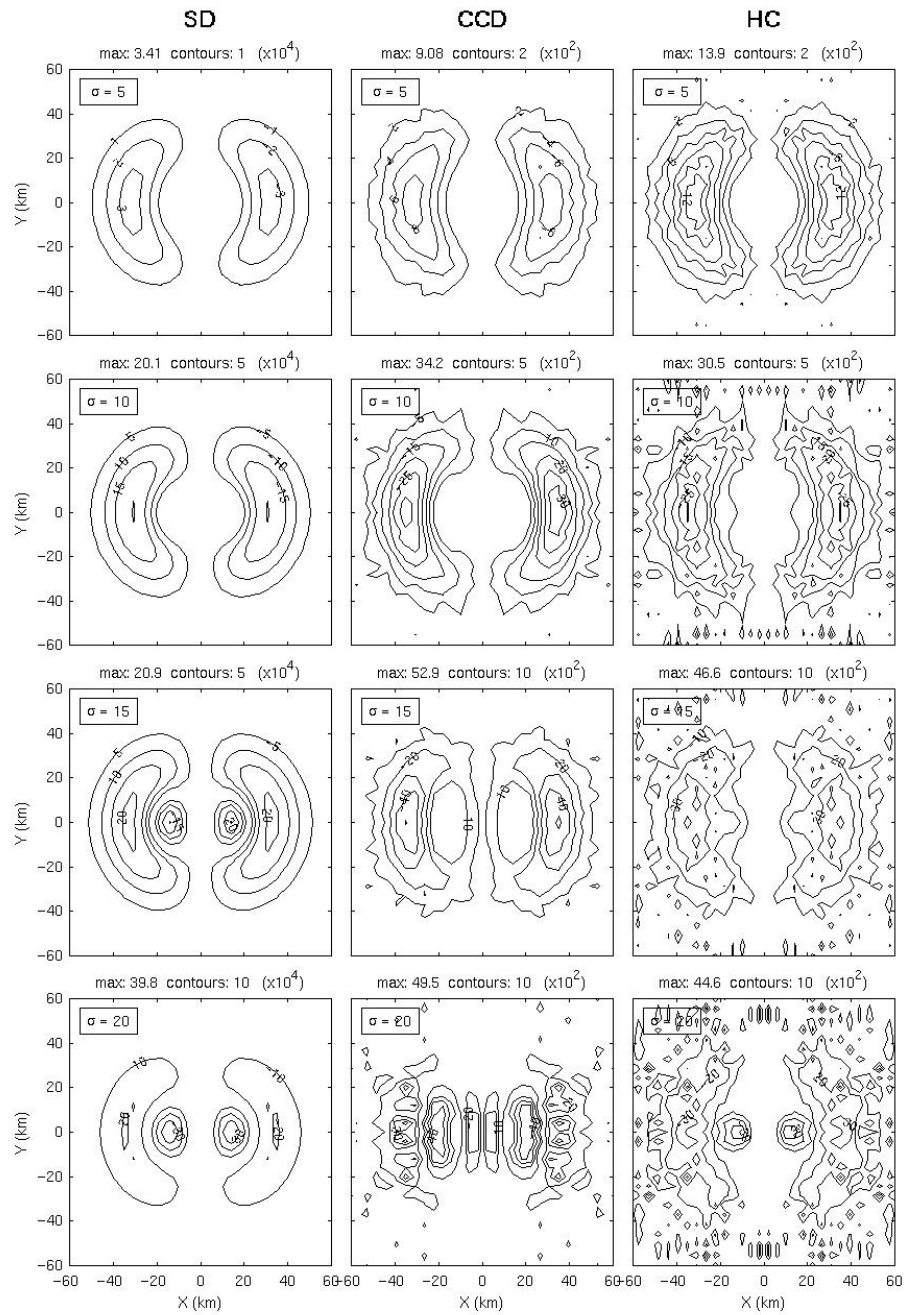


# Verification of Current Schemes by Ezer, Arango, Shchepetkin (OCEMOD, 2002)

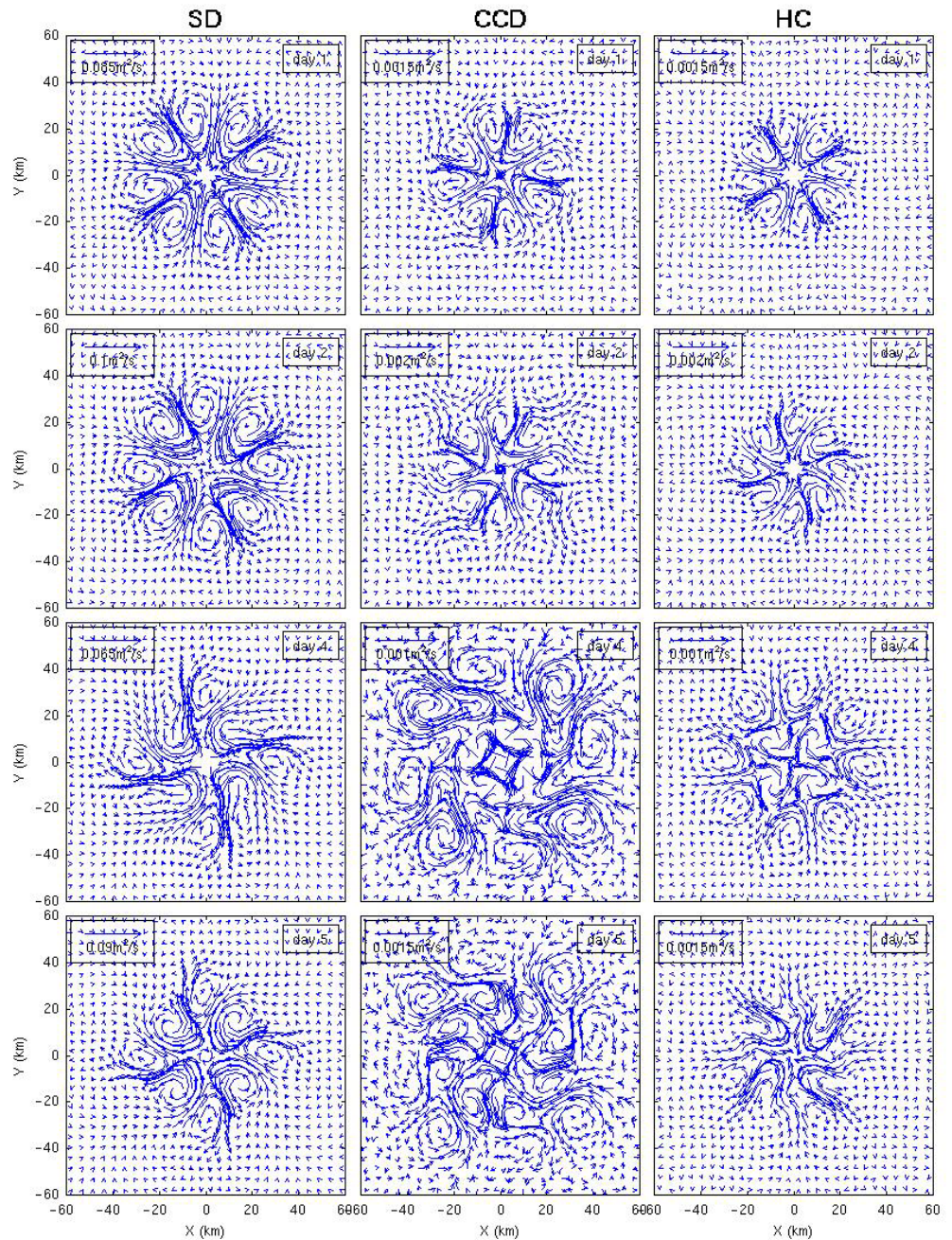


# HC has the same accuracy as CCD Scheme





- HC has the same accuracy as the sixth-order CCD scheme



# CPU time (minute) at the end of 5 day runs of the POM seamount test case using the SD and HC schemes

Scheme	Second-order	HC
CPU Time	171.51	176.92
Ratio	1	1.03

# Conclusions

- Finite volume model combines the strength of z- and sigma-coordinate models.
- Hydrostatic correction scheme is a simple scheme with high accuracy and efficiency.
- The accuracy of the HC scheme is similar to the sixth-order CCD scheme.
- The CPU cost is similar to the ordinary second-order scheme.